



Issues in Dependency Modeling in Multi-Unit Seismic PRA

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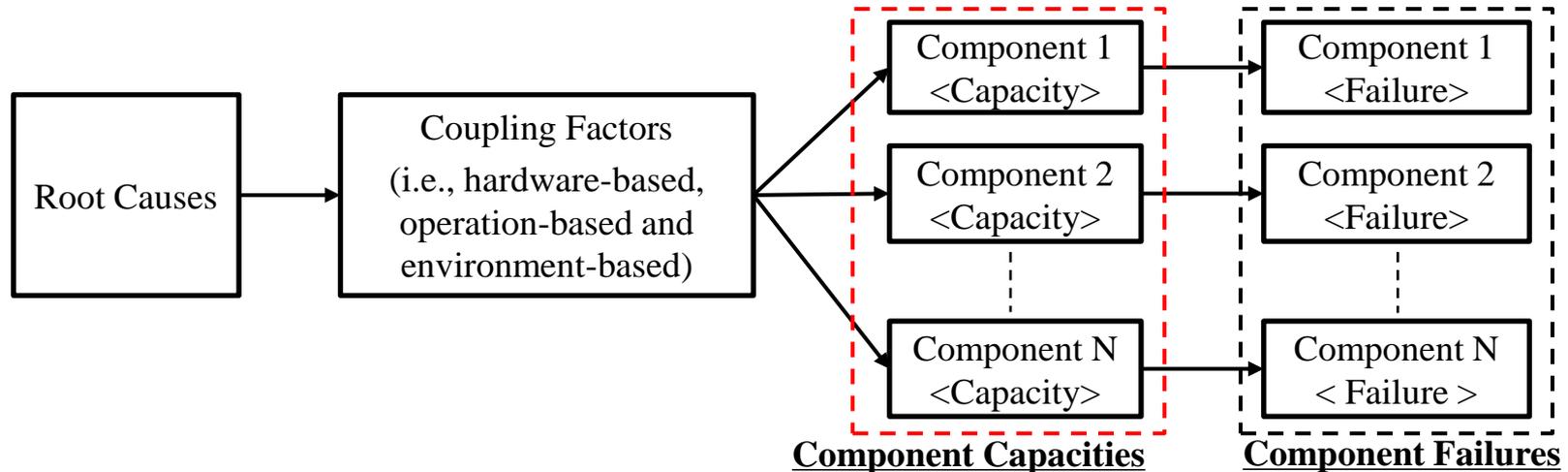


Presentation Overview



- Background and Motivation
- State-of-the-Art on Seismic Dependency Modeling
- Existing Issues with Demonstration
- Conclusions

Background and Motivation



❑ Common Cause Failure (CCF) Models:

- Shock Model and Non-Shock Model.

❑ Recent efforts to enhance the current CCF models:

- Improve the quality of CCF database.
- Formulate a casual CCF model to link relevant sources with Bayesian network.
- Address other limitations, such as improve uncertainty treatment.
- Establish a multi-unit PRA considering dependencies across reactor units, e.g., external events, especially **seismic event**.

State-of-the-Art

□ Current Approaches to Seismic Dependency Modeling:

- 1) Follow the traditional parametric CCF methods in the internal events PRAs.
- 2) Incorporate the dependencies by means of the correlation between seismic failures. (i.e., Seismic Safety Margins Research Program (SSMRP); Mike Bohn's thumb rules).
- 3) Incorporate the dependencies by means of correlation of the ground acceleration capacity.



Proposed by Reed et al., 1985, referred to as Reed-McCann method

- J.W. REED, M.W. MCCANN, JR.J. IIHARA, and H.H. TAMJED. "Analytical Techniques for Performing Probabilistic Seismic Risk Assessment of Nuclear Power Plants," Proc. of the 4th International Conference on Structural safety and reliability, Kobe, Japan, May 27-29 (1985).
- R. J. BUDNITZ, G. S. HARDY, D. L. MOORE and M. K. RAVINDRA. "Correlation of Seismic Performance in Similar SSCs (Structures, Systems, and Components)," Final Report Draft, Lawrence Berkeley National Laboratory, Berkeley, California (2015) (under NRC review)

- 4) Combined methodologies to exploit the features of three approaches above.



Derive the CCF parameter given the correlation coefficient.

- J. U. KLUGEL. "On the treatment of dependency of seismically induced component failures in seismic PRA," *Transactions of the 20th International Conference on Structural Mechanics in Reactor Technology (SMiRT 20)*, Helsinki, Finland, August 9-14 (2009).
- M. PELLISSETTI and U. KLAPP. "Integration of correlation models for seismic failures into fault tree based seismic PSA," *Transactions of the 21st International Conference on Structural Mechanics in Reactor Technology (SMiRT 21)*, New Delhi, India, Nov 6-11 (2011).



State-of-the-Art (cont.)



□ Issues and Challenges:

- Features of dependencies might be altered with different interpretations of seismic hazard, fragility development and reactor design research results.
- Given the features of dependencies available, there are issues in the current methods to quantify joint fragility:
 - (1) Inappropriate equivalence assumption between β -factor and correlation coefficient;
 - (2) Issues in the numerical quantification procedure in the Reed-McCann method.

Hypothesis between β -Factor and Correlation Coefficient

□ An analytical example:

- A parallel system composed of two components A and B.
- The component states: X_A, X_B ; system state: X_{AB} .
- The marginal failure probability P_A, P_B ; joint failure probability P_{AB} .

□ Correlation coefficient ρ_{AB} :

$$\rho_{AB} = \frac{\text{COV}[X_A, X_B]}{\sigma_{X_A} \cdot \sigma_{X_B}} = \frac{E[X_{AB}] - E[X_A] \cdot E[X_B]}{\sigma_{X_A} \cdot \sigma_{X_B}} = \frac{P_{AB} - P_A P_B}{\sqrt{P_A(1 - P_A)P_B(1 - P_B)}}$$

□ Rules (given equivalence assumption works):

- Correlation coefficient is less than the actual β -factor.

$\rho_{AB} < \beta$ lead to non-conservative estimate

- Correlation coefficient is no less than the actual β -factor.

$\rho_{AB} \geq \beta$ lead to conservative estimate

Hypothesis between β -Factor and Correlation Coefficient (cont.)

□ The joint failure probability P_{AB} can be expressed as (assume $P_A = P_B = P$):

1) $P_{AB} = P_A P_B + \rho_{AB} \sqrt{P_A(1 - P_A)P_B(1 - P_B)} = P^2 + \rho_{AB} \cdot P \cdot (1 - P)$

2) $P_{AB} = (1 - \beta)^2 P^2 + \beta \cdot P$

□ Equating equations (1) and (2) to find the analytical relationship between ρ_{AB} and β -factor:

$$P \cdot \beta^2 + (1 - 2P) \cdot \beta - \rho_{AB} \cdot (1 - P) = 0$$

□ The analytical solution provides the actual relationship between the β -factor and ρ_{AB} as:

$$\beta = \frac{(2P - 1) + \sqrt{(1 - 2P)^2 + 4P \cdot (1 - P) \cdot \rho_{AB}}}{2P}$$

Hypothesis between β -Factor and Correlation Coefficient (cont.)

□ Let's assume $\beta < \rho_{AB}$ (ensure conservative estimate), then:

$$\left\{ \begin{array}{l} 0 < \frac{(2P-1) + \sqrt{(1-2P)^2 + 4P \cdot (1-P) \cdot \rho_{AB}}}{2P} < \rho_{AB} \\ 0 < \rho_{AB} \leq 1 \\ 0 < P \leq 1 \end{array} \right. \rightarrow \text{Null solution}$$

□ Let's assume $\beta \geq \rho_{AB}$ (cause non-conservative estimate), then:

$$\left\{ \begin{array}{l} \rho_{AB} \leq \frac{(2P-1) + \sqrt{(1-2P)^2 + 4P \cdot (1-P) \cdot \rho_{AB}}}{2P} \leq 1 \\ 0 < \rho_{AB} \leq 1 \\ 0 < P \leq 1 \end{array} \right. \rightarrow \left\{ \begin{array}{l} 0 < P \leq 1 \\ 0 < \rho_{AB} \leq 1 \end{array} \right.$$

Limitation of Reed-McCann Method

Case No.	Dependency	System Configuration	Description
1	Dependent Components	Intersection of components (3/3)	All three dependent components fail
2		Union of components (1/3)	At least one dependent component fails
3	Independent Components	Intersection of components (3/3)	All three independent components fail
4		Union of components (1/3)	At least one independent component fails

- ❑ Use the example problem from Reed et al. for examination purpose.
- ❑ Examine the performance by comparing the joint fragilities of four different cases.
- ❑ Lack of sufficient benchmarking results (two sets of results exist).
 - 1) Reed et al. presented results for all the four cases, but only for one specific sample set within the ten sample sets generated in total.
 - 2) Budnitz et al. presented results for two dependent cases (i.e., case 1 and case 2) using the same sample set in Reed et al. Results are also provided for ten equally weighted sample sets, while based on one iteration.



Limitation of Reed-McCann Method (cont.)

□ Comparison Study:

- Comparison between the composite fragility curve and mean fragility curve in the independent cases (i.e., case 3; case 4);
- Comparison Between dependent and independent cases (i.e., case 1 vs. case 3; case 2 vs. case 4).

□ Rules:

- 1) Composite fragility curve is equivalent to mean fragility curve.
- 2) The correlation for the intersection cases always increases the tendency of joint failure. $\frac{y_1}{y_3} > 1$
- 3) The correlation for the union cases always reduce the likelihood of joint failure. $\frac{y_4}{y_2} > 1$

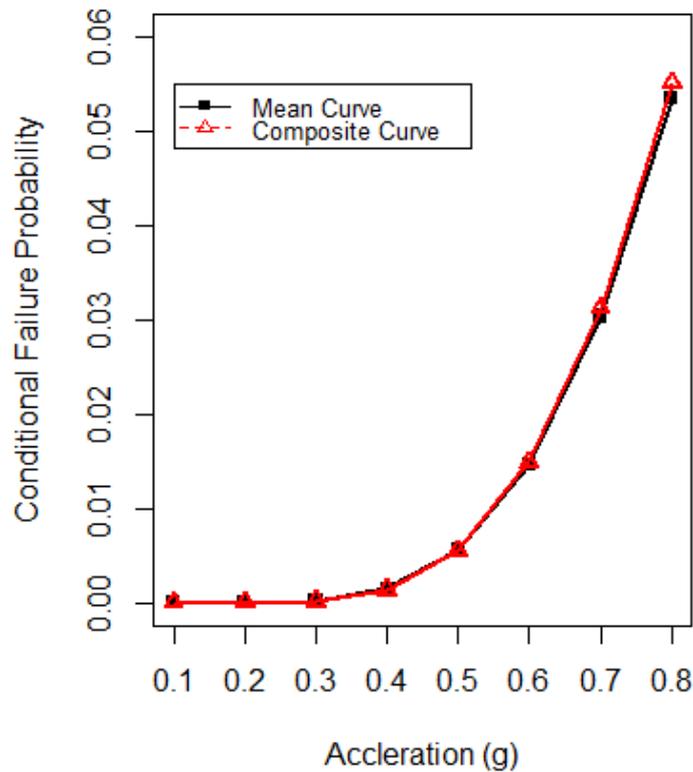
□ Performance index α :

$$\alpha = \frac{\sum_{i=1}^N \left[I\left(\frac{y_1^i}{y_3^i}\right) \cdot I\left(\frac{y_4^i}{y_2^i}\right) \right]}{N} ; i = 1, \dots, N$$

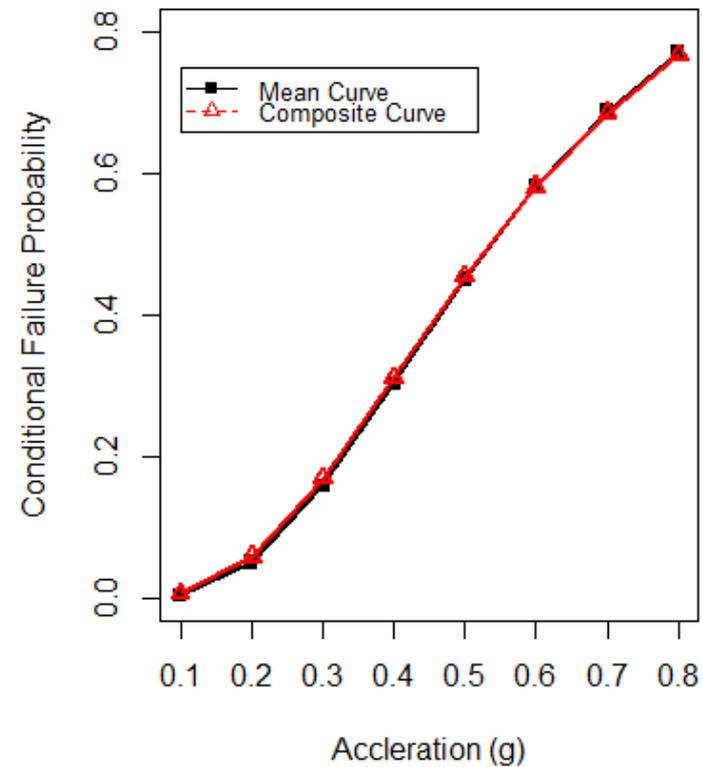


Comparison – Independent Cases

Case 3: Intersection of Three Components Independent



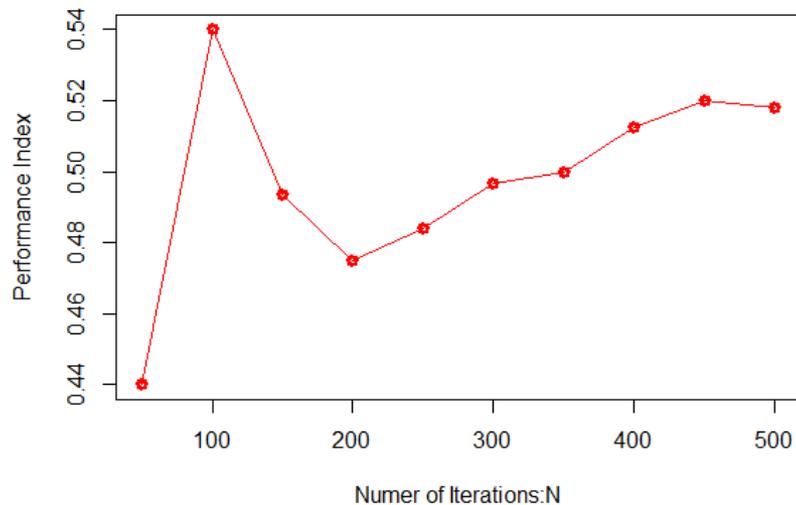
Case 4: Union of Three Components Independent



Comparison – Dependent and Independent Cases

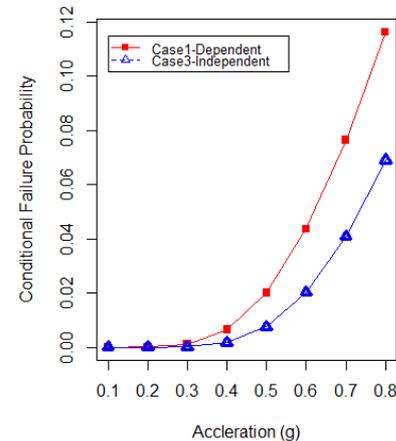
Performance index given ten different numbers of iterations N

Reed-McCann method
Performance Index

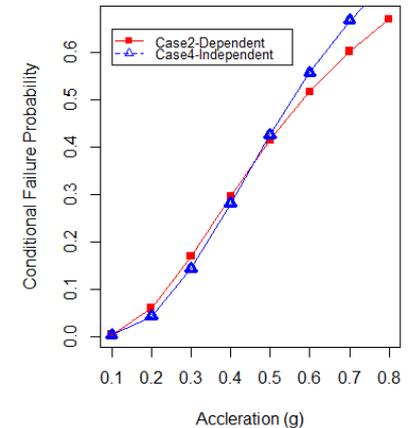


Example results – Intersection & Union
(seed number = 500)

Intersection of Three Components
Case 1 vs. Case 3



Union of Three Components
Case 2 vs. Case 4



Conclusions



- The equivalence hypothesis between the β -factor and correlation coefficient is not appropriate.
- The Reed-McCann method is not performing well to characterize the contribution of dependencies.
- There is a need to develop an improved method for characterizing the SSCs with shared features



Thank You!